E Damped system

E.1 Derivation

This is mostly from Wikipedia³. Take a simple system with a mass, a spring and a damper (figure 1): There are



Figure 1: Mass spring damper system.

three forces:

1. A force from the spring, proportional to displacement

$$f_s = -ky. (162)$$

2. A force from the damper, proportional to velocity

 $f_d = -c \frac{dy}{dt}.$ (163)

3. An (optional) external input force

f_i. (164)

Putting these into Newton's second law,

$$force = mass \times acceleration$$
 (165)

$$f_i - ky - c\frac{dy}{dt} = m\frac{d^2y}{dt^2}$$
(166)

$$m\frac{d^2y}{dt^2} + c\frac{dy}{dt} + ky = f_i$$
(167)

or, writing \boldsymbol{y} as $\boldsymbol{y}(t)$ and \boldsymbol{f}_i and $\boldsymbol{f}(t)$

$$m\ddot{y}(t) + c\dot{y}(t) + ky(t) = f(t).$$
 (168)

The Laplace transform⁴ of this is

$$m [s^{2}Y(s) - sy(0) - \dot{y}(0)] + c [sY(s) - y(0)] + kY(s) = F(s)$$
(169)

$$Y(s)(ms^{2} + cs + k) = msy(0) + m\dot{y}(0) + cy(0) + F(s)$$
(170)

$$w(z) = msy(0) + m\dot{y}(0) + cy(0) + F(s)$$
 (171)

$$\Upsilon(s) = \frac{1}{\mathrm{ms}^2 + \mathrm{cs} + \mathrm{k}}.$$
 (171)

So, there is a single zero and a double pole.

E.2 Reparameterisation

The two poles are at

$$s = \frac{-c \pm \sqrt{c^2 - 4mk}}{2m},\tag{172}$$

³https://en.wikipedia.org/wiki/Damping

⁴https://en.wikipedia.org/wiki/Laplace_transform

and are coincident when $c^2 = 4mk$. Further, when c = 0 the poles are pure imaginary at

$$s = \pm j \sqrt{\frac{k}{m}},\tag{173}$$

at which the system will resonate. Hence, define

$$\zeta^2 \triangleq \frac{c^2}{4mk} \implies c = 2\zeta\sqrt{mk}, \tag{174}$$

and

$$\omega_0^2 \triangleq \frac{k}{m} \implies k = m\omega_0^2.$$
(175)

In this case, the system becomes

$$\ddot{y}(t) + 2\zeta \omega_0 \dot{y}(t) + \omega_0^2 y(t) = f(t)/m.$$
 (176)

Note also that we can define

$$x(t) \triangleq \frac{f(t)}{k} \implies f(t) = kx(t),$$
 (177)

which has the effect of parameterising the force as a distance x(t) being the distance that the spring would move if subjected to f(t). We then have

$$\frac{f(t)}{m} = \frac{k}{m}x(t) = \omega_0^2 x(t)$$
(178)

so

$$Y(s) = \frac{sy(0) + \dot{y}(0) + 2\zeta\omega_0 y(0) + \omega_0^2 X(s)}{s^2 + 2\zeta\omega_0 s + \omega_0^2},$$
(179)

with poles

$$s_1 = -\omega_0 \zeta + \omega_0 \sqrt{\zeta^2 - 1},$$
 (180)

$$s_2 = -\omega_0 \zeta - \omega_0 \sqrt{\zeta^2 - 1},$$
 (181)

or, if $\zeta = 1$ (critical damping)

$$s_1 = s_2 = -\omega_0.$$
 (182)



Figure 2: Damped systems for $\zeta = 1.5, 1$ and 0.1 respectively, and assuming $\dot{y}(0) = 0$ and X(s) = 0.

In general, for the system to do something interesting, it either needs non-zero initial conditions, or some driving force. These are discussed below.



Figure 3: Driven systems: Impulse, step and linear respectively.

E.3 General solutions

E.3.1 General case

We have

$$Y(s) = \frac{sy(0) + \dot{y}(0) + 2\zeta\omega_0 y(0) + \omega_0^2 X(s)}{s^2 + 2\zeta\omega_0 s + \omega_0^2}$$
(183)

with

$$s_1 = -\omega_0 \zeta + \omega_0 \sqrt{\zeta^2 - 1},$$
 (184)

$$s_2 = -\omega_0 \zeta - \omega_0 \sqrt{\zeta^2 - 1}.$$
 (185)

The solution does not have a particularly attractive form:

$$y(t) = \frac{y(0)}{-s_2 + s_1} \left(s_1 e^{s_1 t} - s_2 e^{s_2 t} \right) + \frac{\dot{y}(0) + 2\zeta \omega_0 y(0) + \omega_0^2 X(s)}{-s_2 + s_1} \left(e^{s_1 t} - e^{s_2 t} \right)$$
(186)

$$=e^{-\zeta\omega_0 t}\left[Ae^{\sqrt{\zeta^2-1}\omega_0 t}-Be^{-\sqrt{\zeta^2-1}\omega_0 t}\right]$$
(187)

where

$$A = \frac{\left(\zeta + \sqrt{\zeta^2 - 1}\right)\omega_0 y(0) + \dot{y}(0) + \omega_0^2 X(s)}{2\omega_0 \sqrt{\zeta^2 - 1}}$$
(188)

$$B = \frac{\left(\zeta - \sqrt{\zeta^2 - 1}\right)\omega_0 y(0) + \dot{y}(0) + \omega_0^2 X(s)}{2\omega_0 \sqrt{\zeta^2 - 1}}.$$
(189)

The natural response is obtained for X(s) = 0; the form does not simplify.

E.3.2 Impulse driven

If we assume steady state initial conditions and an impulsive driving force, X(s) = 1, we have

$$Y(s) = \frac{\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}$$
(190)

$$y(t) = \frac{\omega_0}{2\sqrt{\zeta^2 - 1}} e^{-\zeta \omega_0 t} \left(e^{\sqrt{\zeta^2 - 1}\omega_0 t} - e^{-\sqrt{\zeta^2 - 1}\omega_0 t} \right)$$
(191)

and if $\zeta^2 < 1$,

$$=\frac{\omega_0}{\sqrt{1-\zeta^2}}e^{-\zeta\omega_0 t}\sin\left(\sqrt{1-\zeta^2}\omega_0 t\right).$$
(192)

i.e., an exponentially weighted sinusoid.

E.4 Critically damped solutions

E.4.1 Impulse driven

Assuming critical damping and an impulse driving force,

$$Y(s) = \frac{sy(0)}{(s+\omega_0)^2} + \frac{\dot{y}(0) + 2\omega_0 y(0) + \omega_0^2}{(s+\omega_0)^2}$$
(193)

$$y(t) = y(0)(1 - \omega_0 t)e^{-\omega_0 t} u(t) + [\dot{y}(0) + 2\omega_0 y(0) + \omega_0^2]te^{-\omega_0 t} u(t),$$
(194)

$$= (\mathbf{A} + \mathbf{B}\mathbf{t})e^{-\omega_0 \mathbf{t}} \mathbf{u}(\mathbf{t}), \tag{195}$$

where $\boldsymbol{u}(t)$ is the Heaviside step function and

$$A = y(0),$$
 (196)

$$B = \dot{y}(0) + \omega_0 y(0) + \omega_0^2.$$
(197)

For steady state initial conditions,

$$y(t) = \omega_0^2 t e^{-\omega_0 t} u(t).$$
 (198)

E.4.2 Step driven

Assuming critical damping and a step driving force,

$$\mathbf{x}(\mathbf{t}) = \mathbf{b} \tag{199}$$

$$X(S) = \frac{b}{s}$$
(200)

$$Y(s) = \frac{sy(0)}{(s+\omega_0)^2} + \frac{\dot{y}(0) + 2\omega_0 y(0)}{(s+\omega_0)^2} + \frac{b\omega_0^2}{s(s+\omega_0)^2}$$
(201)

$$y(t) = y(0)(1 - \omega_0 t)e^{-\omega_0 t} u(t) + [\dot{y}(0) + 2\omega_0 y(0)]te^{-\omega_0 t} u(t) + b - b(1 + \omega_0 t)e^{-\omega_0 t} u(t),$$
(202)
= $[b - (A + Bt)e^{-\omega_0 t}] u(t),$ (203)

$$A = y(0) + b,$$
 (204)

$$B = \dot{y}(0) + \omega_0(y(0) + b).$$
(205)

For steady state initial conditions and b = 1,

$$y(t) = \left[1 - (1 + \omega_0 t)e^{-\omega_0 t}\right]u(t).$$
(206)

E.4.3 Linear function driven

In this case,

$$\mathbf{x}(\mathbf{t}) = \mathbf{b} + \mathbf{m}\mathbf{t} \tag{207}$$

$$X(s) = \frac{b}{s} + \frac{m}{s^2},$$
 (208)

so it is the step case with extra terms

$$\frac{m\omega_0^2}{s^2(s+\omega_0)^2}$$
 (209)

and

$$-\frac{m}{\omega_0}\left(2-\omega_0 t-(\omega_0 t+2)e^{-\omega_0 t}\right)$$
(210)

SO

$$y(t) = \left[-\frac{2m}{\omega_0} + mt + b - (A + Bt)e^{-\omega_0 t}\right]u(t), \qquad (211)$$

with

$$A = y(0) + b + \frac{2m}{\omega_0},$$
 (212)

$$B = \dot{y}(0) + \omega_0(y(0) + b) + m.$$
(213)

E.5 Discretisation

E.5.1 Impulse driven, general case

First sample the time domain with t = nT,

$$y(t) = \frac{\omega_0}{\sqrt{\zeta^2 - 1}} e^{-\zeta \omega_0 t} \sin\left(\sqrt{\zeta^2 - 1}\omega_0 t\right)$$
(214)

$$y(nT) = \frac{\omega_0}{\sqrt{\zeta^2 - 1}} e^{-\zeta \omega_0 nT} \sin\left(\sqrt{\zeta^2 - 1}\omega_0 nT\right)$$
(215)

$$=\frac{\theta_0^2}{\theta T}r^n \sin(n\theta) \tag{216}$$

where

$$\theta_0 = \omega_0 \mathsf{T},\tag{217}$$

$$\theta = \theta_0 \sqrt{\zeta^2 - 1},\tag{218}$$

$$\mathbf{r} = e^{-\zeta \theta_0},\tag{219}$$

Now transform

$$Y(z) = \frac{\theta_0^2}{\theta T} \frac{r z^{-1} \sin(\theta)}{1 - 2r z^{-1} \cos(\theta) + r^2 z^{-2}}$$
(220)

$$=\frac{\theta_0^2}{\theta T}\frac{rz\sin(\theta)}{(z-re^{j\theta})(z-re^{-j\theta})}.$$
(221)

E.5.2 Impulse driven, critically damped

Sampling is the same as above:

$$y(t) = \omega_0^2 t e^{-\omega_0 t} u(t)$$
(222)

$$y(nT) = \omega_0^2 nT e^{-\omega_0 nT} u(0)$$
(223)

$$=\frac{\theta_0^2}{T}\operatorname{nr}^n\mathfrak{u}(0). \tag{224}$$

Then the transform is also tabulated

$$Y(z) = \frac{\theta_0^2}{T} \frac{rz^{-1}}{(1 - rz^{-1})^2}$$
(225)

$$=\frac{\theta_0^2}{T}\frac{rz}{(z-r)^2}.$$
 (226)

E.5.3 Critically damped natural response from offset

This like the impulse driven case, but with non-zero y(0) and no input:

$$y(t) = (y(0) + \omega_0 y(0)t) e^{-\omega_0 t} u(t)$$
(227)

$$y(nT) = (y(0) + \omega_0 y(0)nT) e^{-\omega_0 nT} u(0)$$
(228)

$$= (y(0)r^{n} + \theta_{0}y(0)nr^{n}) u(0)$$
(229)

$$Y(z) = y(0) \frac{1}{1 - rz^{-1}} + \theta_0 y(0) \frac{rz^{-1}}{(1 - rz^{-1})^2}$$
(230)
(1 + r\theta_0)z = r

$$= y(0) \frac{(1 + r\theta_0)z - r}{(z - r)^2}$$
(231)

E.5.4 Basic exponential decay

This is trivial, but for reference:

$$y(t) = e^{-\omega_0 t} \tag{232}$$

$$y(nT) = e^{-\omega_0 nT}$$
(233)

$$=r^{n}$$
(234)

$$Y(z) = \frac{1}{1 - rz^{-1}}$$
(235)

$$=\frac{z}{z-r}$$
(236)